|             | NATIONAL UNIVERSITY OF SCIENCE AND TECHNOLOGY<br>FACULTY OF INDUSTRIAL TECHNOLOGY<br>DEPARTMENT OF CIVIL AND WATER ENGINEERING<br>STRUCTURAL ANALYSIS I<br>TCW 3102 |
|-------------|---|
| Examination | Paper   |
| December 20 | 16  |
|             | This examination paper consists of 8 pages  |

Time Allowed: 3 hours

Total Marks: 100

**Special Requirements: None** 

Examiner's Name: Miss Diana Makweche/ Mrs Faith Makwiranzou

#### **INSTRUCTIONS**

- 1. Answer any four (4) questions. Credit will not be given for additional questions attempted.
- 2. Each question carries 25 marks.
- 3. Where relevant, use the solution method prescribed.

#### **MARK ALLOCATION**

| QUESTION | MARKS |
|----------|-------|
| 1.       | 25    |
| 2.       | 25    |
| 3.       | 25    |
| 4.       | 25    |
| 5.       | 25    |
| TOTAL    | 100   |

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(i) Analyse the beam in Figure Q1A for reactions, bending moment diagram and shear force diagram.
 [6]



[6]



(ii) Figure Q1B shows two frames. Sketch the deflected shape of each and explain the differences observed.





- (iii) Construct the influence line for truss member CH in the truss of Figure Q1C. (Use the Method of Sections to obtain the truss member forces). [10]
- (iv) What is the maximum compressive force in the member due to a uniformly distributed load of intensity 10kN/m? [3]



The propped cantilever in Figure Q2A experiences a settlement of 12mm at support B under the action of a uniformly distributed load of 15kN/m.

(i) Using the Flexibility Method, determine the reactions. [15] Take  $E = 200GPa (200x10^6 kN/m^2)$  and  $I = 80x10^6 mm^4$ .



(ii) A statically indeterminate truss is to be analysed. Using the information provided in Figure Q2B, construct a table and calculate the truss member forces.  $A = 200mm^2$  and  $E = 200GPa (200x10^6 kN/m^2)$ . [10]



### **QUESTION 3**

Figure Q3 shows a frame of constant flexural rigidity (EI).

(i) Sketch the deflected shape, and clearly indicate the angles through which the joints rotate.

| (ii)  | Find the magnitude of the fixed end moments.                        | [2]  |
|-------|---|------|
| (iii) | Determine the member end moments using the Slope Deflection Method. | [10] |
| (iv)  | Calculate the reactions.  | [4]  |
| (v)   | Construct the bending moment and shear force diagrams.              | [6]  |



The beam of Figure Q4 is fully fixed at the end supports A and D; and continuous over internal supports B and C.  $E = 200GPa (200x10^{6}kN/m^{2})$ .

| (i)   | Calculate the stiffness factors.  | [3] |
|-------|---|-----|
| (ii)  | Determine the distribution factors.   | [3] |
| (iii) | Find the fixed end moments.   | [2] |
| (iv)  | Use the Moment Distribution Method to determine the end moments in each span. | [7] |
| (v)   | Determine the reactions.  | [4] |
| (vi)  | Draw the bending moment and shear force diagrams.                             | [6] |

(vi) Draw the bending moment and shear force diagrams.



Figure Q5 shows a continuous beam that is fixed at one end, A, and sits on rollers at B and C. Using two beam elements of equal length

| (i)   | Determine the equivalent nodal forces at the end of each element                    | [4]   |
|-------|---|-------|
| (1)   |   | L ' J |
| (11)  | Construct the stiffness matrix for each element.                                    | [4]   |
| (iii) | Assemble the global stiffness matrix.   | [5]   |
| (iv)  | Reduce the global system of equations by applying the boundary conditions.          | [4]   |
| (v)   | Calculate the unknown displacements and the forces at the ends of the elements and, |       |
|       | hence, the reactions.   | [8]   |
|       |   |       |



# Integral Table

| 15<br>15<br>15                           |  | L.  | F.  |  | E E                       |         |   |
|--|--|---|---|--|---------------------------|---------|---|
| $\frac{L}{2}mM$                          | $\frac{L}{2}mM$  | $\frac{L}{2}mM$                           | $\frac{L}{2}mM$                           | $\frac{L}{2}(m_L + m_R)M$  | LmM                       | M       |   |
| $\frac{L}{4}m(M_L + M_R)$                | $\frac{L}{6}m\left[M_L\left(1+\frac{b}{L}\right) + M_R\left(1+\frac{a}{L}\right)\right]$ | $\frac{L}{6}m(M_L+2M_R)$                  | $\frac{L}{6}m(2M_L+M_R)$                  | $\frac{L}{6} [m_L (2M_L + M_R) + m_R (M_L + 2M_R)]$  | $\frac{L}{2}m(M_L + M_R)$ |         | c |
| $\frac{L}{4}mM$                          | $\frac{L}{6}m\left(1+\frac{b}{L}\right)M$  | $\frac{L}{6}mM$                           | $\frac{L}{3}mM$                           | $\frac{L}{6}(2m_L + m_R)M$   | $\frac{L}{2}mM$           | , ⊥ , M |   |
| $\left(\frac{3L^2-4c^2}{12dL}\right)LmM$ | $\frac{(L^2 - a^2 - c^2)}{6bc}LmM$ only for $a < c$                                      | $\frac{L}{6}m\left(1+\frac{c}{L}\right)M$ | $\frac{L}{6}m\left(1+\frac{d}{L}\right)M$ | $\frac{L}{6} \left[ m_L \left( 1 + \frac{d}{L} \right) + m_R \left( 1 + \frac{c}{L} \right) \right] M$ | $\frac{L}{2}mM$           | L M     |   |
| $\frac{L}{3}mM$                          | $\left(\frac{3L^2-4a^2}{12bL}\right)LmM$   | $\frac{L}{4}mM$                           | $\frac{L}{4}mM$                           | $\frac{L}{4}(m_{L}+m_{R})M$  | $\frac{L}{2}mM$           | м       |   |
| $\frac{7L}{48}mM$                        | $\frac{L}{12}m\left(1+\frac{b}{L}+\frac{b^2}{L^2}\right)M$                               | $\frac{L}{12}mM$                          | $\frac{L}{4}mM$                           | $\frac{L}{12}(3m_L + m_R)M$  | $\frac{L}{3}mM$           | L       |   |
| $\frac{17L}{48}mM$                       | $\frac{L}{12}m\left(5-\frac{a}{L}\right)$ $-\frac{a^2}{L^2}M$                            | $\frac{L}{4}mM$                           | $\frac{5L}{12}mM$                         | $\frac{L}{12}(5m_L + 3m_R)M$   | $\frac{2L}{3}mM$          | M<br>L  |   |

To Evaluate Product Integrals of the Form:  $\int_0^L mMdx$ 

TCW 3102

(Caprani C- Lecture Notes)

**Fixed End Moments** 



# **Slope Deflection Equations**

$$M_N = 2Ek(2\theta_N + \theta_F - 3\psi) + (FEM)_N$$

$$M_N = 3Ek(\theta_N - \psi) + (FEM)_N$$

**Beam Stiffness Matrix** 

$$\begin{cases} f_{1y} \\ m_1 \\ f_{2y} \\ m_2 \\ \end{cases} = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix} \begin{cases} v_1 \\ \phi_1 \\ v_2 \\ \phi_2 \\ \end{cases}$$

# **Equivalent Nodal Forces**

|                           |                           | $m_1$  |                           |                      |
|---------------------------|---------------------------|--|---------------------------|----------------------|
| Equivale                  | nt Nodal Forces for Diffe | erent Load Types   | Positive nodal force c    | conventions $f_{2y}$ |
| $f_{1y}$                  | $m_1$                     | Loading case   | $f_{2y}$                  | $m_2$                |
| $\frac{-P}{2}$            | $\frac{-PL}{8}$           | $\frac{L}{2} \qquad P \qquad \frac{L}{2}$  | $\frac{-P}{2}$            | $\frac{PL}{8}$       |
| $\frac{-Pb^2(L+2a)}{L^3}$ | $\frac{-Pab^2}{L^2}$      | $\begin{array}{c c} a & \downarrow^{P} & b \\ \hline & L \\ (a < b) \end{array}$ | $\frac{-Pa^2(L+2b)}{L^3}$ | $\frac{Pa^2b}{L^2}$  |
| - <i>P</i>                | $-\alpha(1-\alpha)PL$     | $ \begin{array}{c} P \\ P \\ \alpha L \\ L \\ L \end{array} $                    | - <i>P</i>                | $\alpha(1-\alpha)PL$ |
| $\frac{-wL}{2}$           | $\frac{-wL^2}{12}$        |  | $\frac{-wL}{2}$           | $\frac{wL^2}{12}$    |
| $\frac{-7wL}{20}$         | $\frac{-wL^2}{20}$        |  | $\frac{-3wL}{20}$         | $\frac{wL^2}{30}$    |

(Logan D L- A First Course in the Finite Element Method)